

# Broadband from the Sky- welche Satelliten brauchen wir dafür?



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Sky-Cell

Georg  
Strauß

Status

Constellation

Target

UP-Link

DOWN-  
Link

Coverage

Blue 3

Conclusions

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- 1 Status Cell Coverage
- 2 Parameter of Constellation
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- 4 UP-Link: Satellite Antenna as Receiver
- 5 DOWN-Link: Satellite Antenna as Transmitter
- 6 Beam Coverage
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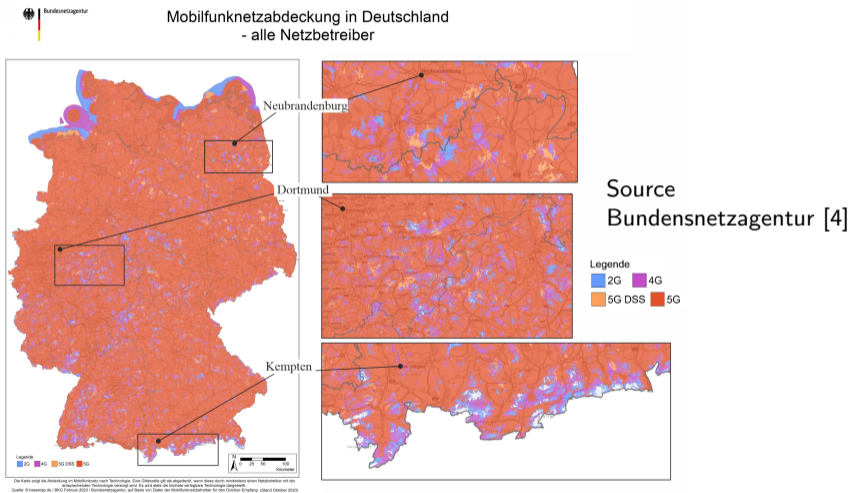
Coverage

Blue 3

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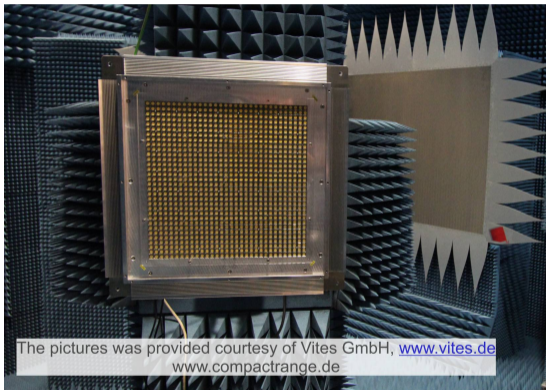
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# VITES Ku-Band

Example of a High End Terrestrial SatCom Antenne



- 1024 active elements
- steering angle up to 60°
- full programmable arbitrary polarization

## RX Performance

$$G/T > 10 \text{ dB(K}^{-1}\text{)}$$

Target is to close gaps using **unmodified cell phones**  
 As example see **T-Mobile US and SpaceX**, Satellite System MARS-ULS  
 or **Vodafone and AST Space Exploration**, Satellite System Blue Walker 3

## 2. Liste deutscher Satellitennetzanmeldungen (Umlaufende Systeme) bei der ITU (Stand 03/2023) List of German Satellite filings (non-geo systems) at the ITU (dated 03/2023)

Satellitensysteme Satellite Network	Orbitdaten Orbital Plane	Uplink (R) (Erde-Weltraum) (Earth-to-Space)	Downlink (E) (Weltraum-Erde) (Space-to-Earth)	Week.-Circ./ Spec.-Sect	Datum Date
<b>MARS-ULS</b>	288 Orbitschichten Polar- und Inclined Orbit 340-614 km 29988 Satelliten	614-960 MHz 1427-1518 MHz 1675-1980 MHz 2010-2025 MHz 2110-2170 MHz 2300-2483.5 MHz 2500-2690 MHz	614-960 MHz 1427-1518 MHz 1610-1610.6 MHz 1626.5-1645.5 MHz 1656.5-1660.5 MHz 1670-2025 MHz 2110-2170 MHz 2300-2483.5 MHz 2500-2690 MHz	2984/API/A/13167	23.08.2022
		2049 – 2060 MHz			

Extract from [3]

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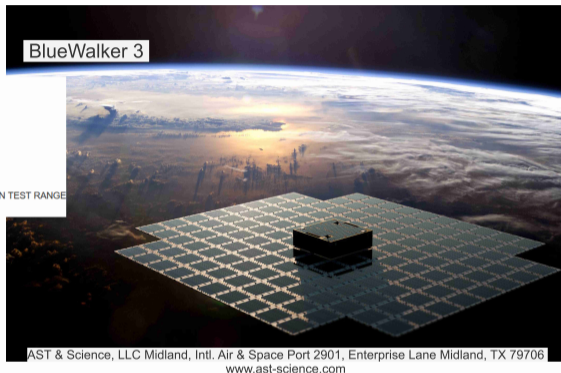
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NORAD ID: 53807  
Int'l Code: 2022-111A  
**Perigee: 494.8 km**  
**Apogee: 508.5 km**  
**Inclination: 53.2°**  
Period: 94.5 minutes  
Semi major axis: 6872 km  
RCS: Unknown  
Launch date: [September 11, 2022](#)  
Source: United States (US)  
Launch site: AIR FORCE EASTERN TEST RANGE  
(AFETR)

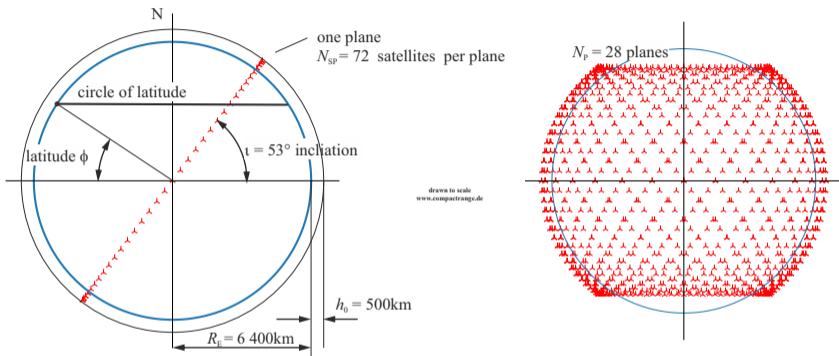


Extract from [2]. Some Technical for MARS-ULS you find in *Attachment A, SpaceX's German-licensed direct to cellular System, December 2022*, [6] and more actual in *Request for Special Authority to Conduct Experimental operations, December 2023* [5].



# Assumptions: Constellation Configuration

Example SapceX Gen2, Equatorial View

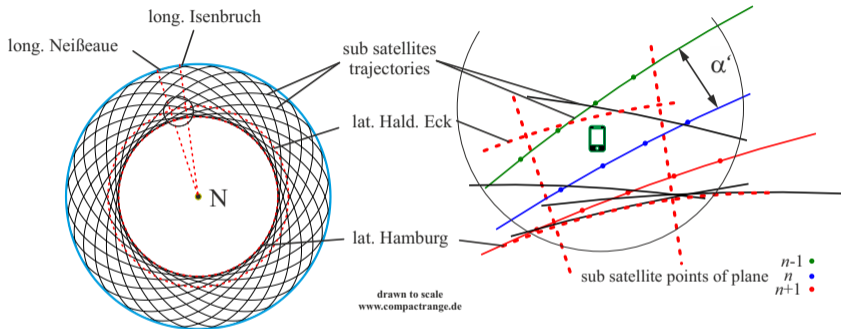


$$N = N_P \cdot N_{SP} = 2016 \text{ satellites}$$

Data from [6]

# Assumptions: Constellation Configuration

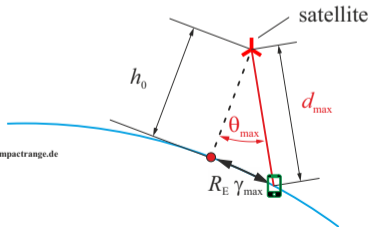
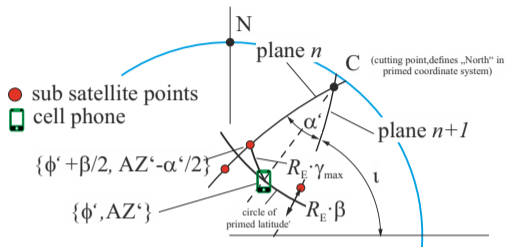
Example SpaceX Gen2, Polar View



Cite (1) Status See space Exploration

# Free Space distance and Satellite's Scan Angle

Some spherical geometry ...



$d_{\max}$  and  $\theta_{\max}$

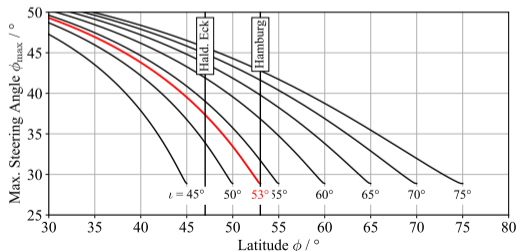
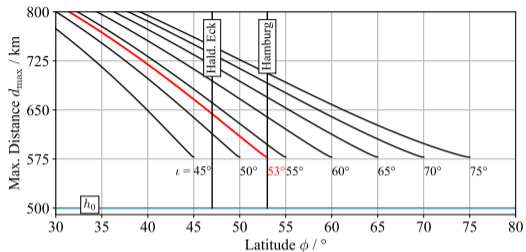
$\phi$ : latitude of cell phone, somewhere in Germany between Haldenwanger Eck, lat.  $47^\circ$  and Hamburg, lat.  $53^\circ$

$\iota$ :  $53^\circ$ , inclination of each plane

$\alpha'$ :  $\approx 10.3^\circ < N_{\text{sat. per plane}}/360^\circ$

$\beta$ :  $360^\circ/N_{\text{sat. per plane}} = 360^\circ/72 = 5^\circ$

$h_0$ : 500 km, satellite flight height



Somewhere in Germany between Haldenwanger Eck / Hamburg and Neißenaue / Isenbruch

Result  $d_{\max}$  and  $\theta_{\max}$

$$500 \text{ km} \leq d \leq 648 \text{ km}$$

$$0 \leq \theta \leq 37.5^{\circ}$$

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## Target Performance Sat2Cell and Cell2Sat

Bit Rate	$R_b$	$10 \text{ Mbit s}^{-1}$
Bit Error Probab.	$P_{er}$	$1 \times 10^{-5}$

## Modulation and Noise Type

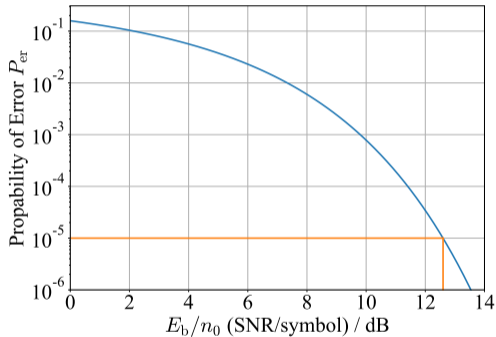
Coherent Frequency Shift Key Modulation (FSK)

Orthogonal Signals

Additive White Gaussian Noise



$$\frac{E_b}{n_0} = 12.6 \text{ dB}$$



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Parameter	Symbol	Value
Frequency Range		1850 MHz to 1910 MHz
Mid. Frequency	$f_{up}$	1880 MHz
Mid. Wavelength	$\lambda_{up}$	0.16 m
Bandwidth	$\Delta f$	10 MHz
Modulation		FSK, coherent
Bandwidth Efficiency	$R_b/\Delta f$	1
Ouput Power Level	$L_{TXup}$	0 dB(W)
Part. real. antenna Gain (lin.)	$G_{TXup}$	-1 dB

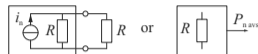
## TX for UP

Free Space Loss	$FSL_{up} = 154.2 \text{ dB}$	$= 20 \lg \left( \frac{4\pi d_{max}}{\lambda_{up}} \right) \text{ dB}$
Equiv. Rad. Pow. Level	$EIRP_{up} = -1 \text{ dB(W)}$	$= L_{TXup} + G_{TXup}$



Available Noise Power

$$P_{n \text{ avs}} = \frac{1}{4} R \langle i_n^2 \rangle$$



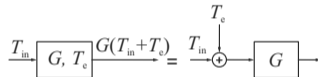
Noise Temperature

$$T = P_{n \text{ avs}} / (k_B \Delta f)$$



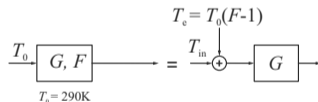
2-Port:  
Equivalent Noise Temperature

$$T_{\text{out}} = (T_{\text{in}} + T_e) G$$



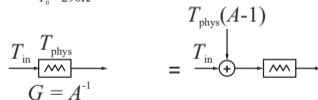
Noise Figure

$$T_e = T_0 (F - 1)$$



Passive 2-Port with physical  
Temperature

$$T_e = T_{\text{phys}} (A - 1)$$

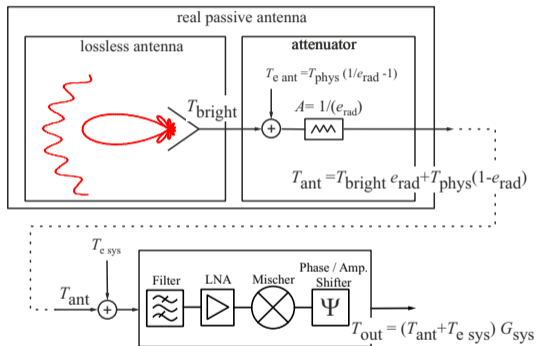


Brightness  $T_{\text{bright}}$  of receiving antenna results from its directivity  $D$  and background radiation  $T_{\text{back}}$  seen by the antenna.

$$T_{\text{bright}} = \frac{\int_{4\pi} T_{\text{back}}(\Omega) D(\Omega) d\Omega}{\int_{4\pi} D(\Omega) d\Omega}$$

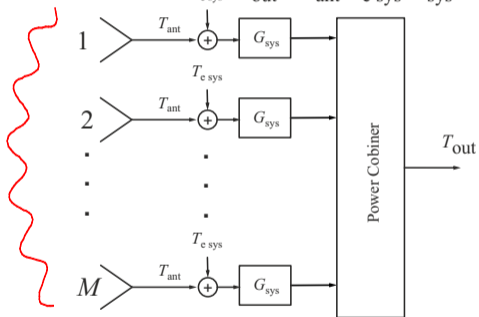
Worst case: Sat. antenna sees only "hot" earth with surface temperature  $T_{\text{earth}} < 300 \text{ K} = 27^\circ \text{C}$

$$T_{\text{bright}} \approx 300 \text{ K}$$



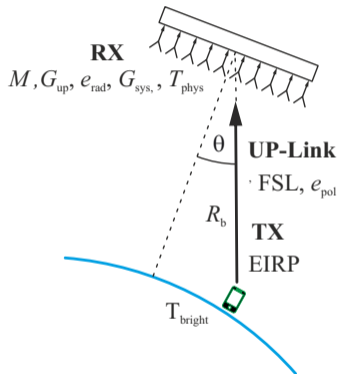
$$T_{\text{ant}} = T_{\text{bright}} e_{\text{rad}} + T_{\text{phys}}(1 - e_{\text{rad}})$$

$$T_{\text{out}} = (T_{\text{ant}} + T_{\text{e sys}}) G_{\text{sys}}$$



Phased Array Antenna,  $M$  similar active antenna blocks:  
Combiner adds only coherent signals!

$$\frac{T_{\text{out}}}{G_{\text{sys}}} = M T_{\text{bright}} e_{\text{rad}} + M T_{\text{phys}} (1 - e_{\text{rad}}) + M T_{\text{e sys}}$$



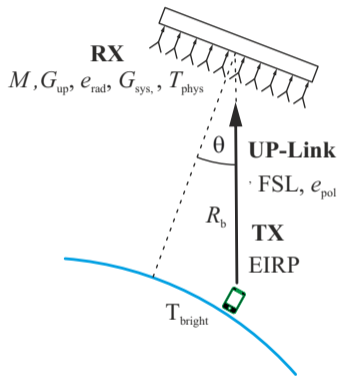
Received Signal Power:

$$\frac{P_{s \text{ RXup}}}{G_{sys \text{ up}}} = \frac{\text{EIRP}_{up} e_{pol \text{ up}}}{\text{FSL}_{up}} \underbrace{M G_{element}}_{G_{RXup,estimated}} \cos(\theta)$$

Received Noise Power:

$$\frac{P_{n \text{ RXup}}}{G_{sys \text{ up}}} = k_B R_b \underbrace{(T_{bright} e_{rad} + T_{phys} (1 - e_{rad}) + T_{e \text{ sys}})}_{T_{up}} \Big|_{RX}$$

$$\Rightarrow \frac{E_B}{N_0} = \frac{1}{k_B R_b} \frac{G_{RXup}}{T_{up}} \frac{\text{EIRP}_{up} e_{pol \text{ up}}}{\text{FSL}_{up}} \cos(\theta)$$



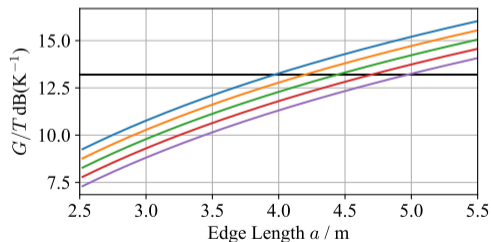
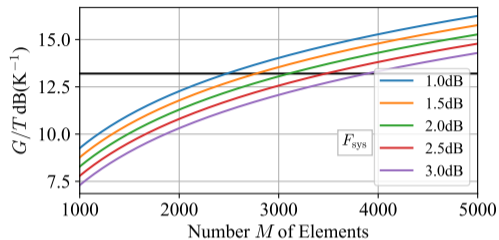
$$\frac{G_{RXup}}{T_{up}} = \frac{E_B}{N_0} k_B R_b \frac{FSL_{up}}{EIRP_{up}} \frac{1}{\epsilon_{pol\ up}} \frac{1}{\cos(\theta_{max})}$$

or with numbers in Dezibel

$$\begin{aligned} \frac{G_{RXup}}{T_{up}} &= 12.6 \text{ dB} + (-228.6 \text{ dB(W Hz}^{-1}\text{K}^{-1})) + 70 \text{ dB(Hz)} \\ &\quad + 154.2 \text{ dB} - (-1 \text{ dB(W)}) + 3 \text{ dB} + 1.0 \text{ dB} \\ &= 13.2 \text{ dB(K}^{-1}) \end{aligned}$$

Cell Phone	EIRP	-1	dB(W)
Free Space	FSL	154.1	dB
	$e_{\text{pol}}$	-3	dB
	$\theta_{\text{max}}$	37.5°	
Satellite	$D_{\text{element}}$	6	dB(ic)
	$e_{\text{rad}}$	-1	dB
	$T_{\text{bright}}$	300	K
	$F_{\text{sys}}$	?	dB
	$T_{\text{phys}}$	300	K
	$M$	?	
	$\lambda_{\text{up}}/2$	80	mm

$$G/T = 13.2 \text{ dB(K}^{-1}\text{)}$$



**$M$  and  $a$** 

Prerequisite for UP-link data rate of  $10 \text{ Mbit s}^{-1}$  with unmodified cell PCS-phone is a phased array antenna with

$$G/T = 13.2 \text{ dB(K}^{-1}\text{)}$$

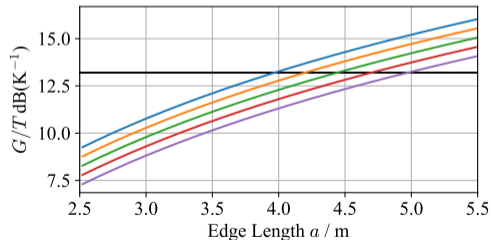
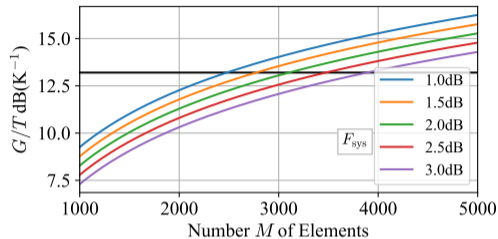
$$1 \text{ dB} < F_{\text{sys}} < 3 \text{ dB}$$

$$2460 < \text{Number of elements } M < 3860$$

$$3.9 \text{ m} < \text{edge length } a < 4.9 \text{ m}$$

$$38.9 \text{ dB} < G_{\text{RXup}} < 40.9 \text{ dB}$$

Square lattice with period  $\frac{1}{2}\lambda_{\text{up}} \Rightarrow$  antenna's edge length is  $a = \sqrt{(M)} \frac{1}{2}\lambda_{\text{up}}$



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# Unmodified Cell Phone, Down-Link: Satellite to Cell Phone

Assumptions for PCS / LTE Band

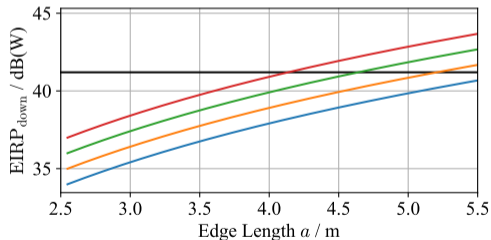
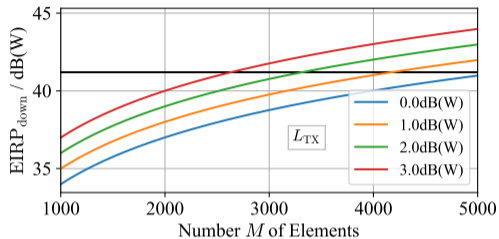
Parameter	Symbol	Value
Frequency Range		1930 MHz to 1990 MHz
Mid. Frequency	$f_{\text{down}}$	1960 MHz
Mid. Wavelength	$\lambda_{\text{down}}$	0.153 m
Bandwidth	$\Delta f$	10 MHz
Modulation		FSK, coherent
Bandwidth Efficiency	$R_b / \Delta f$	1
Directivity	$D_{\text{RXdown}}$	0 dB(i)
Radiation Efficiency	$e_{\text{rad TXup}}$	-1 dB
Pol. Efficiency	$e_{\text{pol down}}$	-3 dB
Noise Figure	$F_{\text{sys down}}$	3 dB
Free Space Loss	FSLdown	154.5 dB

**EIRP<sub>down</sub>**

Given	$G/T$	-28.7 dB(K <sup>-1</sup> )
Required	<b>EIRP</b>	<b>41.2 dB(W)</b>

Cell Phone	$G/T$	$-28.7 \text{ dB(K}^{-1}\text{)}$
Free Space	FSL	154.4 dB
	$e_{\text{pol}}$	-3 dB
	$\theta_{\text{max}}$	$37.5^\circ$
Satellite	$D_{\text{element}}$	6 dB(ic)
	$e_{\text{rad}}$	-1 dB
	$L_{\text{TX}}$	? dB(W)
	$M$	?
	$\lambda_{\text{up}}/2$	80 mm

$EIRP = 41.2 \text{ dB(W)}$



**M and a**

Prerequisite for Down-link data rate of  $10 \text{ Mbit s}^{-1}$  with unmodified cell PCS-phone is a phased array antenna with

$$\text{EIRP}_{\text{down}} = 41.2 \text{ dB(W)}$$

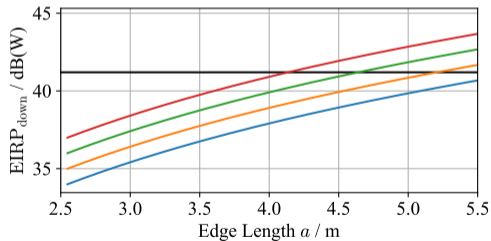
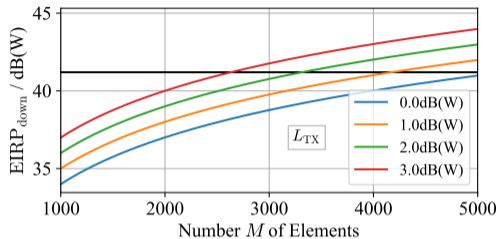
$$0 \text{ dB(W)} < L_{\text{TXdown}} < 3 \text{ dB(W)}$$

$$5255 > \text{Number of elements } M > 2634$$

$$5.8 \text{ m} > \text{edge length } a > 4.1 \text{ m}$$

$$42.2 \text{ dB} < G_{\text{TXdown}} < 39.2 \text{ dB}$$

Square lattice with period  $\frac{1}{2}\lambda_{\text{up}} \Rightarrow$  antenna's edge length is  $a = \sqrt{(M)} \frac{1}{2}\lambda_{\text{up}}$



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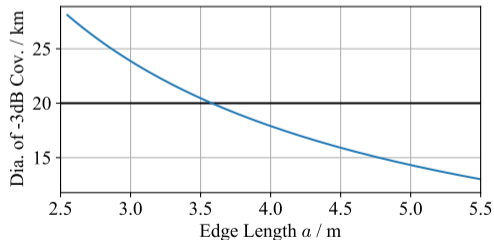
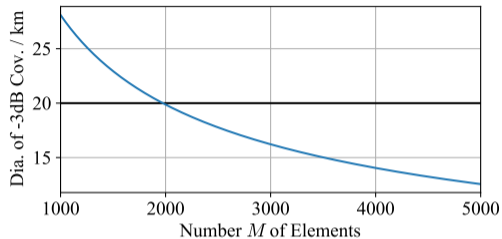
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For half power beamwidth we approximate  
(untapered array)

$$\theta_{\text{HPBW}} = \sqrt{\frac{41\,253}{D_{\text{sat}}}}$$

and find as diameter  $\varnothing_{-3\text{dB}}$  of the  $-3\text{ dB}$ -coverage

$$\varnothing_{-3\text{dB}} = 2 h_0 \tan \theta_{\text{HPBW}}$$



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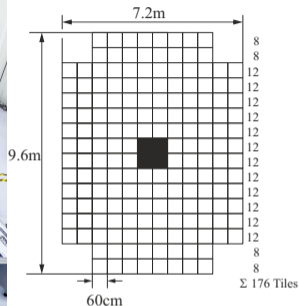
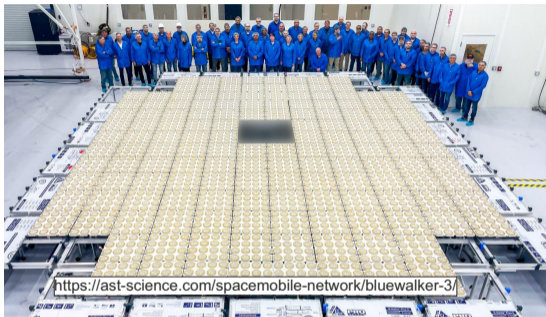
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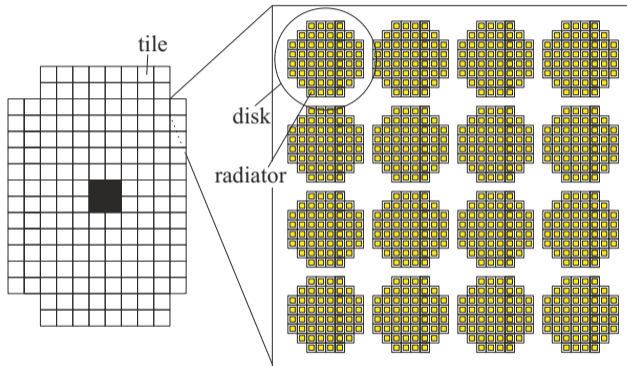
Information found in [1]

Active area is 693 feet<sup>2</sup>, 176 tiles counted

$$\Rightarrow 693 \text{ feet}^2 \approx 176 \text{ tiles} \cdot \frac{(2 \text{ feet})^2}{\text{tile}}$$

size of on tiles is 2 feet  $\times$  2 feet  $\approx$  60 cm  $\times$  60 cm

**Outer dimensions  $\approx$  9.6 m  $\times$  7.2 m**



There are

$$(52-2) \frac{\text{radiators}}{\text{disk}} \times 8 \frac{\text{disks}}{\text{tile}} \times (176-4) \text{tiles}$$

$$= 68\,800 \text{radiators}$$



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# Requirements for Satellites

Comparison of estimated data with data from sources

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To achieve an up- and down-link with  $R_b = 10 \text{ Mbit s}^{-1}$  at PCS-frequencies (approx. 2000 MHz) between unmodified cell phone and constellation with 2016 satellites and 500 km-height requires Satellites phased array antennas with:

parameter	estimated	found in [5], [6]
EIRP	$> 41.2 \text{ dB(W)}$	49 dB(W) to 58 dB(W)!
$L_{\text{TX}}$	$\approx 3 \text{ dB(W)}$	?
$\varnothing_{-3 \text{ dB}}$	15 km to 20 km	33 km
$G/T$	$\approx 13.2 \text{ dB(K}^{-1}\text{)}$	up to 12.5 dB(K <sup>-1</sup> )
$F_{\text{sys}}$	$\approx 1 \text{ dB}$	?
$D_{\text{element}}$	6 dB(ic)	?
$e_{\text{rad}}$	-1 dB	?
pitch	80 cm	?
$M$	$\approx 2500$	?
$a \times a$	$< 4 \text{ m} \times 4 \text{ m}$	$< 8 \text{ m} \times 6 \text{ m}$
$G$	39 dB(ic) to 41 dB(ic)	29 dB(ic) to 39 dB(ic)

Yes, it is possible to close the white spots worldwide with internet from the sky!

Unmodified cell phones can do it.

We “only” need the satellite technology to support it.

It already happens, let's do it ourselves!

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Questions and comments are welcome!

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- 7 Blue Walker 3
- 8 Conclusions
- 9 References**



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